HIGH POWER QUAD OPERATIONAL AMPLIFIER

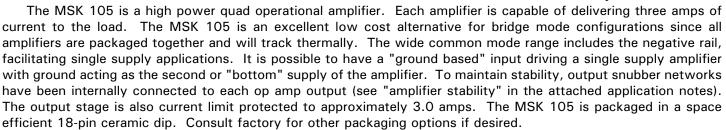
M.S.KENNEDY CORP.

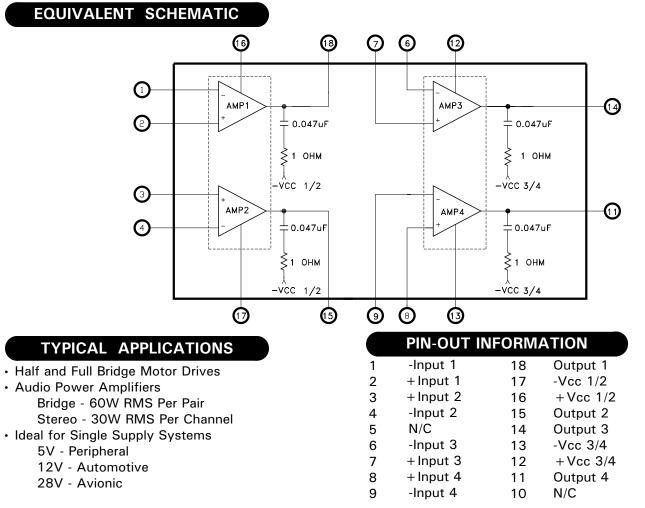
4707 Dey Road Liverpool, N.Y. 13088

FEATURES:

- Low Cost
- Wide Supply Voltage Range: 5V to 40V
- High Output Current: 3A Minimum
- High Efficiency: Vs-2.2V at 2.5A
- Internal Current Limit
- Wide Common Mode Range (Includes Negative Supply Voltage)
- Low Distortion
- · Internal Output Snubbers for Ultra-Stable Operation

DESCRIPTION:







MIL-PRF-38534 CERTIFIED

ABSOLUTE MAXIMUM RATINGS

Vcc	Total Supply Voltage 40V	Тsт	Storage Temperature65°C to +150°C
± І оит	Output Current (within S.O.A.) 4A	TLD	Lead Temperature
VIND	Input Voltage (Differential) $\dots \dots \dots \pm Vcc$	Tc	Case Operating Temperature
Vin	Input Voltage		(MSK105B)
	(Common Mode) + Vcc, -Vcc-0.5V		(MSK105)
TJ	Junction Temperature	Rтн	Thermal Resistance (DC)
			Junction to Case

(Per Amplifier).

4.0°C/W

ELECTRICAL SPECIFICATIONS

Parameter	Test Conditions (1)	Group A	Г	MSK105B			MSK105		
Falailletei		Subgroup	Min.	Тур.	Max.	Min.	Тур.	Max.	Units
TATIC									
Supply Voltage Range (2)	(Split Supply)	-	±2.5	±15	±20	±2.5	±15	±20	V
		1	-	±60	±150	-	±60	±150	mA
Quiescent Current	Total; $V_{IN} = 0V$	2	-	±120	±210	-	-	-	mA
		3	-	±40	±150	-	-	-	mA
NPUT									
Offset Voltage	VIN = OV	1	-	±0.5	±12	-	±2	±15	mV
Offset Voltage Drift ②	VIN = OV	-	-	±15	-	-	±15	-	μV/°C
Input Bias Current (2)	Vcm=0V	-	-	±35	±1000	-	±35	±1500	nA
	Full Temp.	-	-	±75	±1000	-	±75	-	nA
Power Supply Rejection 2	$\Delta Vcc = \pm 15V$	-	60	80	-	60	80	-	dB
Common Mode Rejection (2)	$V_{CM} = \pm 10 VDC$	-	60	85	-	60	85	-	dB
Total Noise	$R_L \!=\! 500\Omega \hspace{0.1in} A_V \!=\! 1 \hspace{0.1in} C_L \!=\! 1500 p F$	-	-	0.1	1.0	-	0.1	1.0	mV
OUTPUT									
Output Voltage Swing	$(IOUT = \pm 0.5A)$	4	±14	±14.2	-	±14	±14.2	-	V
Output Current	Vout=MAX	4	±3.0	±4.0	-	±3.0	±4.0	-	А
Current Limit ②		-	-	±4.0	-	-	±4.0	-	А
Power Bandwidth ②	Vout = 28Vpp	-	-	13.6	-	-	13.6	-	KHz
Crosstalk	IOUT = 1A f = 1KHz	-	60	68	-	-	68	-	dB
Capacitive Load ②	Av = + 1V/V	-	-	0.022	-	-	0.022	-	μF
RANSFER CHARACTERISTICS									
Slew Rate		4	0.5	1.5	-	0.5	1.5	-	V/µS
Open Loop Voltage Gain (2) $f = 10Hz RL = 500\Omega$		-	80	100	-	80	100	-	dB

NOTES:

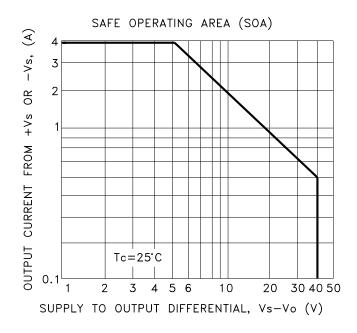
- Unless otherwise noted ±VCC = ±15VDC. Specification is for each amplifier.
 Devices shall be capable of meeting the parameter, but need not be tested. Typical parameters are for reference only.
 Industrial grade devices shall be tested to subgroups 1 and 4 unless otherwise requested.
 Military grade devices ('B' suffix) shall be 100% tested to subgroups 1,2,3 and 4.
 Subgroup 5 and 6 testing available upon request.
 Subgroup 1 4. TC = ±25°C

Subgroup 1,4 TC = +25 °C

Subgroup 2,5 TC = +125 °C

Subgroup 3,6 TA = -55 °C

SAFE OPERATING AREA (SOA)



Safe operating area curves are a graphical representation of all of the power limiting factors involved in the output stage of an operational amplifier. Three major power limiting factors are; output transistor wire bond carrying capability, output transistor junction temperature and secondary breakdown effects. To see if your application is meeting or exceeding the limitations of the safe operating area curves, perform the following steps:

1.) Find the worst case output power dissipation. For a split supply, purely resistive load application, this occurs when VOUT = 1/2 Vcc.

2.) Take the values of (Vcc-Vout) and the corresponding output current and find their intersection on the safe operating area curves.

3.) Verify this point is below the safe operating area curves.

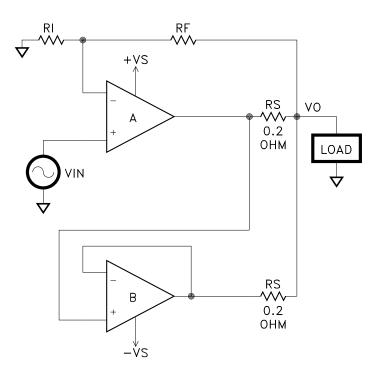
This is a simple task for purely resistive loads, for reactive loads the following table will save extensive analysis. Under transient conditions, capacitive and inductive loads up to the following maximum are safe.

± Vcc	Capacitive Load	Inductive Load
20V	200uF	7.5mH
15V	500uF	25mH
10V	5mF	35mH
5V	50mF	150mH

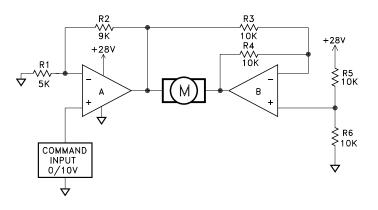
If the inductive load is driven near steady state conditions allowing the output to drop more than 6V below the supply rail while the amplifier is current limiting, the inductor should be capacitively coupled or the supply voltage must be lowered to meet the SOA criteria. It is a good practice to also connect reverse biased fast recovery diodes to the output for protection against sustained high energy flyback.

AMPLIFIER STABILITY

Since both output transistors in this amplifier are NPN, consideration must be taken when stabilizing the output. A one ohm resistor, 0.047uF capacitor snubber network has been added internally from the output to -Vcc on each amplifier. This configuration minimizes local output stage oscillations. As always, adequate power supply bypassing is a necessity for amplifier stability. A parallel combination of a 4.7uF electrolytic (for every amp of output current) and a 0.01uF ceramic disc capacitor should be connected as close as possible to the package power supply pins to ground. The R-C snubber networks shown on the outputs of the amplifiers in the typical circuits are internal and should not be added externally.







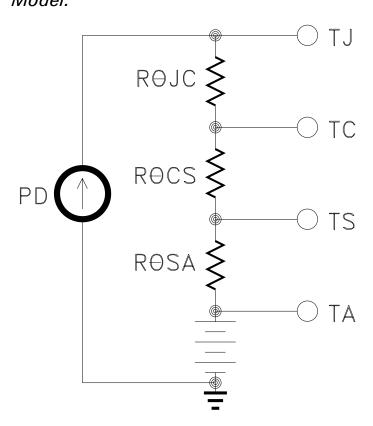
BIDIRECTIONAL MOTOR DRIVE

APPLICATION NOTES CONTINUED

HEAT SINKING

To determine if a heat sink is necessary for your application and if so, what type, refer to the thermal model and governing equation below.

Thermal Model:



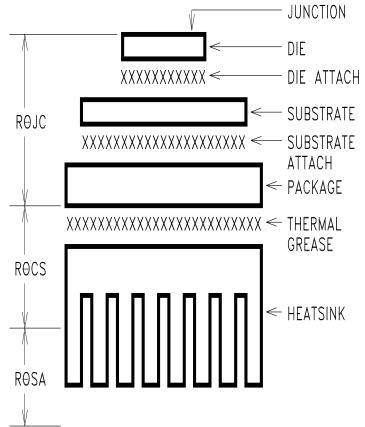
Example:

Inside the MSK 105 package are two monolithic dual amplifiers. For this thermal analysis, each die will be considered individually. In our example the amplifier application requires each output to drive a 10 volt peak sine wave across a 20 ohm load for 0.5 amp of output current. For a worst case analysis we will treat the 0.5 amp peak output current as a D.C. output current. The power supplies are \pm 20VDC.

- 1.) Find Driver Power Dissipation
 - PD = [(quiescent current) x (+Vcc (-Vcc))] + [(Vcc-Vo) x lout x 2]
 - $= (75mA) \times (40V) + (10V) \times (0.5A) + (10V) \times (0.5A)$
 - = 3W + 10W = 13W
- 2.) For conservative design, set $T_J = +150^{\circ}C$.
- 3.) For this example, worst case TA = +25 °C
- 4.) $R_{\theta JC} = 4.0 \,^{\circ}C/W$ typically
- 5.) Recs = $0.15 \,^{\circ}C/W$ for most thermal greases
- 6.) Rearrange governing equation to solve for R $_{ ext{BSA}}$ R $_{ ext{BSA}} = ((T_J - T_A)/P_D) - (R_{ ext{BJC}}) - (R_{ ext{BCS}})$ $= ((150^{\circ}C - 25^{\circ}C) / 13W) - (4^{\circ}C/W) - (.15^{\circ}C/W)$ $\cong 5.5^{\circ}C/W$

The heat sink in this example must have a thermal resistance of no more than 5.5 °C/W to maintain a junction temperature of no more than +150 °C.

Thermal Path:

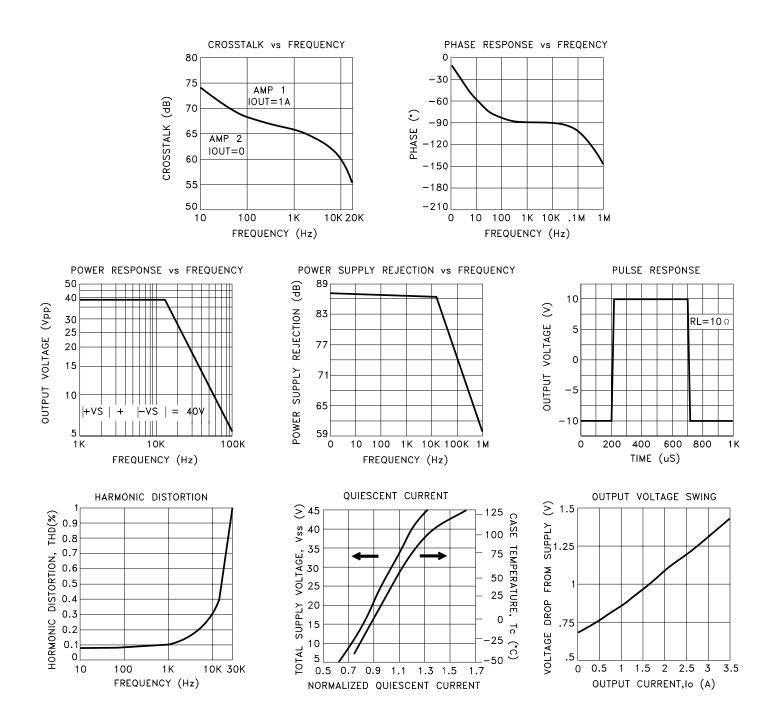


Governing Equation:

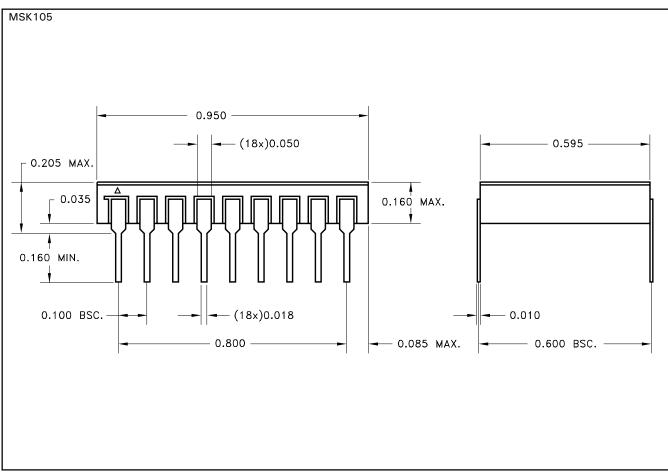
$$T_J = P_D x (R_{\theta JC} + R_{\theta CS} + R_{\theta SA}) + T_A$$

Where

- T_J = Junction Temperature
- PD = Total Power Dissipation
- $R_{\theta JC}$ = Junction to Case Thermal Resistance
- $R\theta CS = Case to Heat Sink Thermal Resistance$
- $R_{\theta SA}$ = Heat Sink to Ambient Thermal Resistance
- Tc = Case Temperature
- TA = Ambient Temperature
- Ts = Sink Temperature



MECHANICAL SPECIFICATIONS



 $\label{eq:solution} \begin{array}{c} \text{ESD TRIANGLE INDICATES PIN 1.} \\ \text{ALL DIMENSIONS ARE } \pm 0.010 \text{ INCHES UNLESS OTHERWISE LABELED.} \end{array}$

ORDERING INFORMATION

Part Number	Screening Level
MSK105	Industrial
MSK105B	Military-Mil-PRF-38534

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